



Fields and Waves I

Lecture 2

Sine Waves on Transmission Lines

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Materials from other sources are referenced where they are used.
Those listed as Ulaby are figures from Ulaby's textbook.

Overview

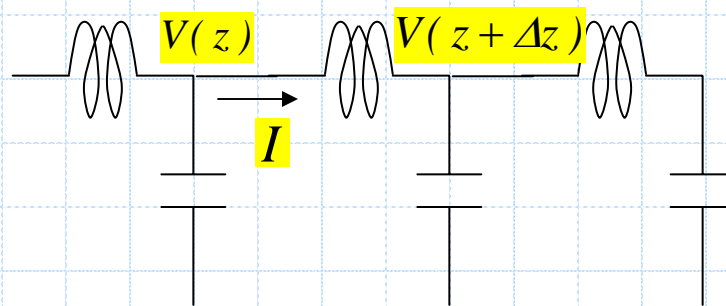


Henry Farny *Song of the Talking Wire*

- Review
- Voltages and Currents on Transmission Lines
- Standing Waves
- Input Impedance
- Lossy Transmission Lines
- Low Loss Transmission Lines

Transmission Line Representation

As $\Delta z \Rightarrow 0$ limit



$$V(z + \Delta z) - V(z) = -L \frac{\partial I}{\partial t} \Rightarrow -l \cdot \frac{\partial I}{\partial t} = \frac{\Delta V}{\Delta z} = \frac{\partial V}{\partial z}$$

$l \cdot \Delta z$

$$\frac{\partial V}{\partial z}$$

Transmission Line Representation

Similarly, $\frac{\partial I}{\partial z} = -c \cdot \frac{\partial V}{\partial t}$ looks like $\frac{\partial V}{\partial z} = -l \cdot \frac{\partial I}{\partial t}$

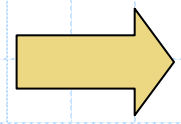
$$\frac{\partial^2 V}{\partial z^2} = \frac{\partial}{\partial z} \left(-l \cdot \frac{\partial I}{\partial t} \right) = -l \cdot \frac{\partial}{\partial t} \left(\frac{\partial I}{\partial z} \right) = lc \frac{\partial^2 V}{\partial t^2}$$

Obtain the following PDE:

$$\frac{\partial^2 V}{\partial z^2} = lc \frac{\partial^2 V}{\partial t^2}$$

$\frac{1}{v^2}$
Wave Eqn
 $\frac{1}{s^2}$

$$\frac{\partial^2}{\partial z^2} \rightarrow \frac{1}{m^2}$$

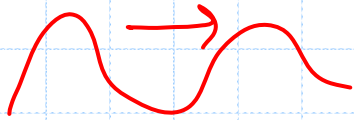


Solutions are:

$$f\left(t \pm \frac{z}{u}\right)$$

$$\frac{s^2}{m^2}$$

These are functions that move with velocity u



Transmission Line Representation

$$\beta = \frac{\omega}{u}$$

Functions that move with velocity u

Example:

$$\cos\left(\omega t \pm \frac{\omega}{u} z\right)$$

$$V = V^+ \cos(\omega t - \beta z) + V^- \cos(\omega t + \beta z)$$

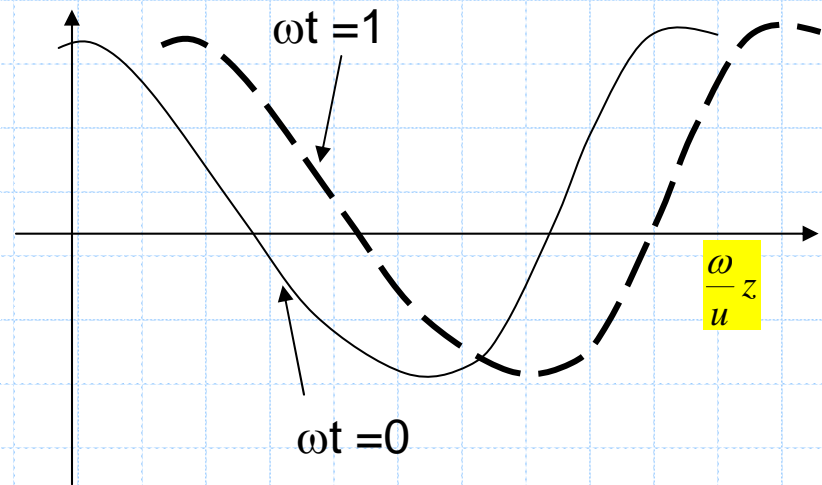
At $t=0$,

$$\cos\left(-\frac{\omega}{u} z\right)$$

Wave moving to the right

At $\omega t = 1$

$$\cos\left(1 - \frac{\omega}{u} z\right)$$



Workspace – look at the general form of the solution

$$\frac{\partial^2 f}{\partial z^2} = \epsilon c \frac{\partial^2 f}{\partial t^2}$$

$$f\left(t \pm \frac{z}{u}\right)$$
$$f\left(t - \frac{z}{u}\right)$$

$$\frac{\partial f}{\partial z} = f' \left(-\frac{1}{u} \right)$$

$$\frac{\partial f}{\partial t} = f' \rightarrow \boxed{\uparrow}$$

$$\frac{\partial^2 f}{\partial t^2} = f'' \left(\frac{1}{u^2} \right)$$

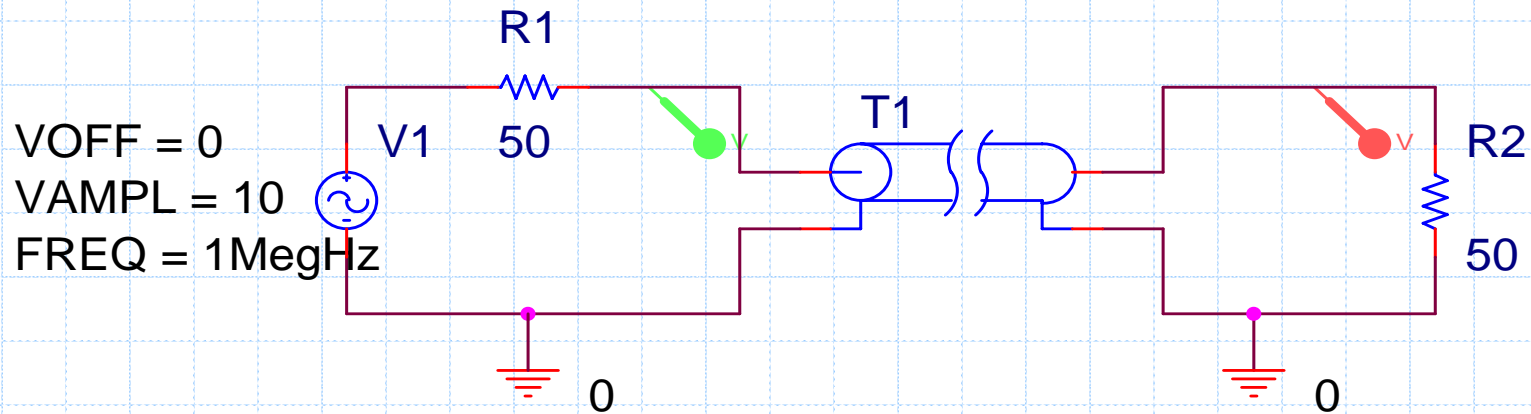
$$\frac{\partial^2 f}{\partial t^2} = f''$$

$$\frac{1}{u^2} = \epsilon c$$

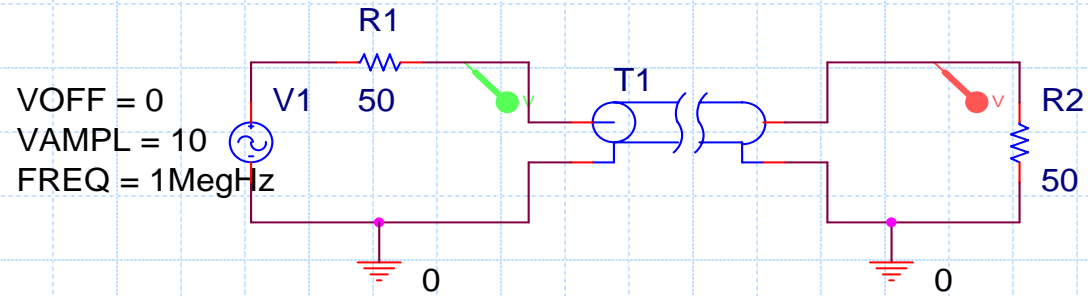
or $u = \frac{1}{\sqrt{\epsilon c}}$

Some Numerical Experiments

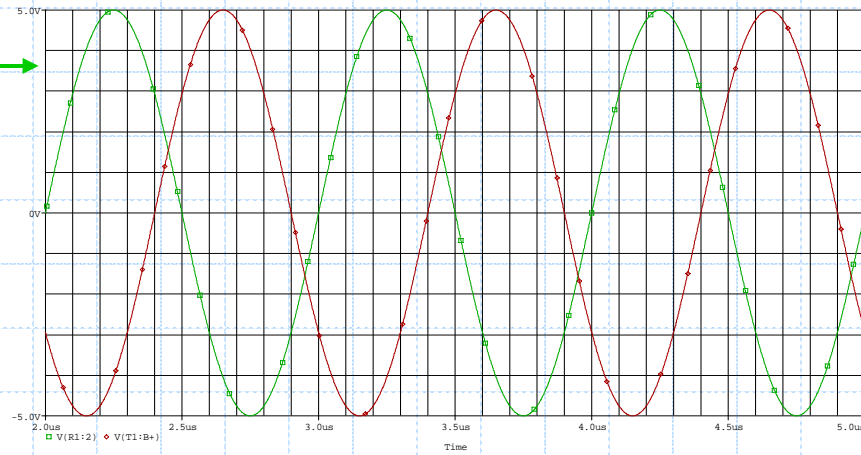
- PSpice can be used to do simple numerical experiments that demonstrate how transmission lines work



PSpice



INPUT



OUTPUT

t

Computer-Based Tools



- When you use a program like PSpice, applets, or any handy tools available online ... remain skeptical.
- Do not assume that the answers are correct.
- Apply crude plausibility checks.
- Know the assumptions and limitations of the tools you are using.
- Test all tools on problems you can solve other ways or with tools you have already tested.
- Use even sometimes incorrect tools as long as errors are recognized.

Pig from <http://www.cincinnati skeptics.org>

PSpice Example

- Let us return to the configuration shown above and simulate it using PSpice
- List some conclusions from this exercise.
 - ?
 - ?
 - ?

Sine Waves

- The form of the wave solution

$$A \cos\left(\omega t \mp \frac{\omega}{u} z\right) = A \cos(\omega t \mp \beta z)$$

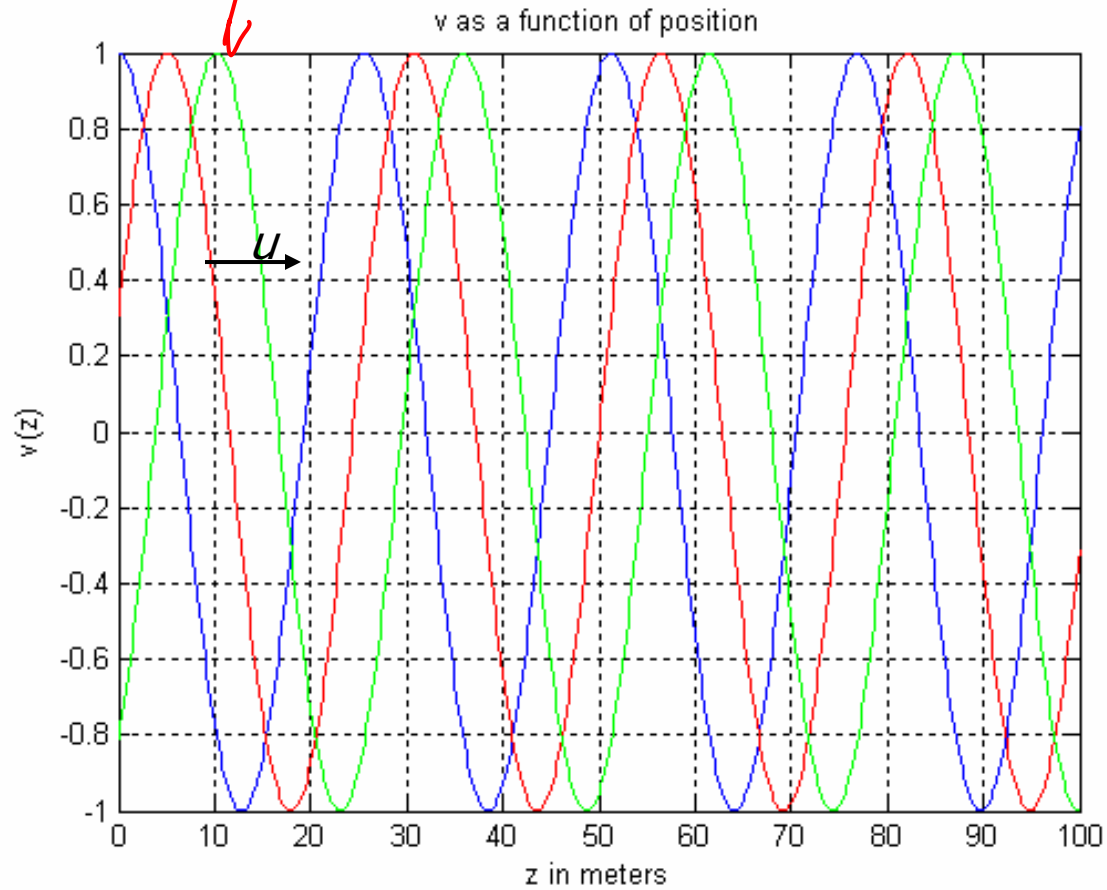
- First check to see that these solutions have the properties we expect by plotting them using a tool like Matlab

Sine Waves

- The positive wave

Apply frequency and wavelength analogy argument to show this is reasonable

$$\cos\left(\omega t - \frac{\omega}{u} z\right) = \cos\left(2\pi f t - \frac{2\pi f}{u} z\right)$$



Solutions to the Wave Equation

- Thus, our sine wave is a solution to the voltage or current equation

$$\frac{\partial^2 V}{\partial z^2} = lc \frac{\partial^2 V}{\partial t^2}$$

- if $\beta = \frac{\omega}{u} = \omega\sqrt{lc}$ or $u = \frac{1}{\sqrt{lc}}$ $u = \frac{\omega}{\beta}$
- $u =$ the speed of wave propagation = the speed of light

Sine Waves

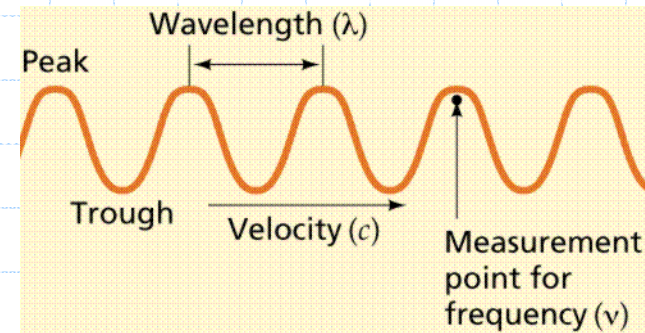
$$\cos\left(\omega t - \frac{\omega}{u} z\right) = \cos\left(2\pi f t - \frac{2\pi f}{u} z\right)$$

- Consider one other property. What is the distance required to change the phase of this expression by 2π ? We just did this qualitatively.
- This distance is called the wavelength or

$$\beta z = \frac{\omega}{u} z = \frac{2\pi f}{u} z = 2\pi$$

$$\beta\lambda = \frac{\omega}{u} \lambda = \frac{2\pi f}{u} \lambda = 2\pi \qquad \lambda = \frac{2\pi}{\beta} = \frac{u}{f}$$

Sine Waves -- Summary



- Solutions look like $A \cos(\omega t \mp \beta z)$

$$\beta = \frac{\omega}{u} = \omega \sqrt{lc} = \omega \sqrt{\mu \epsilon} = \frac{2\pi}{\lambda}$$

$$\omega = 2\pi f = \frac{2\pi}{T}$$

$$\lambda = \frac{2\pi}{\beta} = \frac{u}{f}$$

$$u = \frac{1}{\sqrt{lc}} = \frac{1}{\sqrt{\mu \epsilon}}$$

$$\epsilon = \epsilon_r \epsilon_0 \quad \mu = \mu_r \mu_0$$

Figure from <http://www.emc.maricopa.edu/>

Phasor Notation

$$e^{j\omega t} = \cos \omega t + j \sin \omega t$$

$$e^{j\theta} = \cos \theta + j \sin \theta$$

- For ease of analysis (changes second order partial differential equation into a second order ordinary differential equation), we use phasor notation.

$$f(z, t) = A \cos(\omega t \mp \beta z) = \text{Re}\left(\left\{ A e^{\mp j\beta z} \right\} e^{j\omega t}\right)$$

- The term in the brackets is the phasor.

$$f(z) = A e^{\mp j\beta z}$$
$$V = V^+ e^{-j\beta z} + V^- e^{+j\beta z}$$

Phasor Notation

- To convert to space-time form from the phasor form, multiply by $e^{j\omega t}$ and take the real part.

$$f(z, t) = \text{Re}(Ae^{\mp j\beta z} e^{j\omega t}) = A \cos(\omega t \mp \beta z)$$

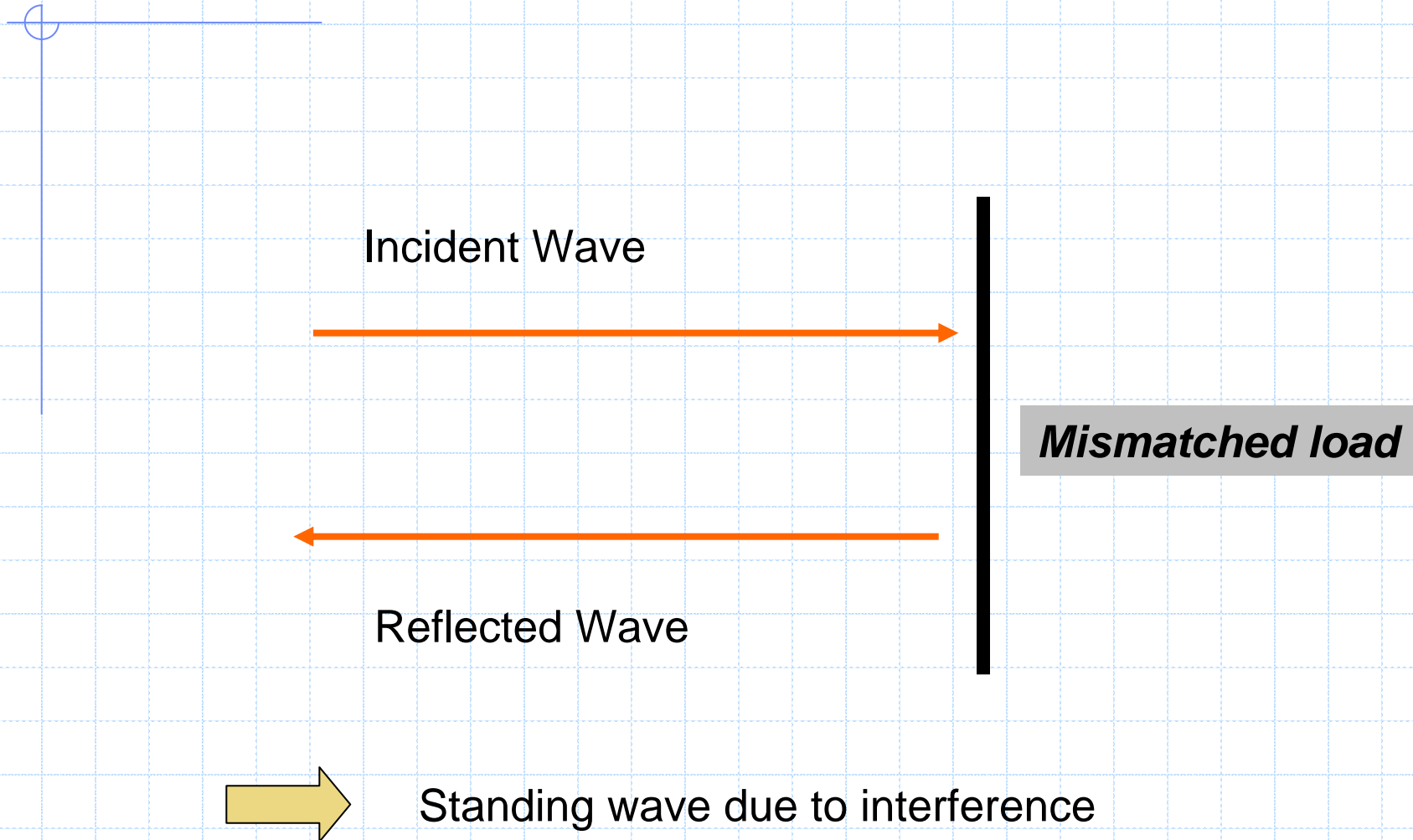
- If A is complex

$$A = |A|e^{j\theta_A}$$

$$f(z, t) = \text{Re}(|A|e^{j\theta_A} e^{\mp j\beta z} e^{j\omega t}) = |A| \cos(\omega t \mp \beta z + \theta_A)$$

$$\text{Re } e^{j\theta} = \cos \theta$$

Transmission Lines



Standing Waves

Reflectometer Calculator

Type a value in one of the fields below and hit 'enter:'

Reflection Coefficient

SWR

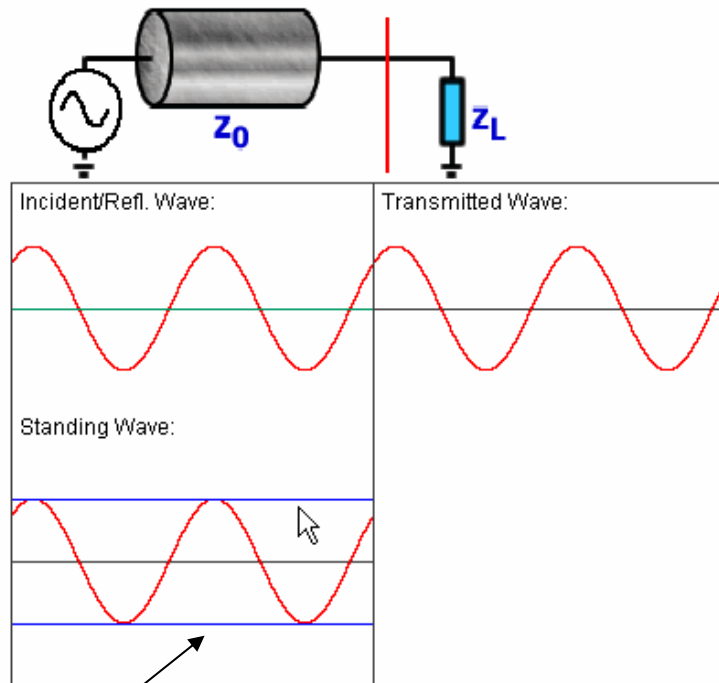
Return Loss (dB)

Mismatch Loss (dB)

Z1

er1

Show two interfaces



<http://www.bessernet.com>

No Standing Wave

[Besser Associates](http://www.bessernet.com)

Standing Waves

Reflectometer Calculator

Type a value in one of the fields below and hit 'enter:'

Reflection Coefficient

SWR

Return Loss (dB)

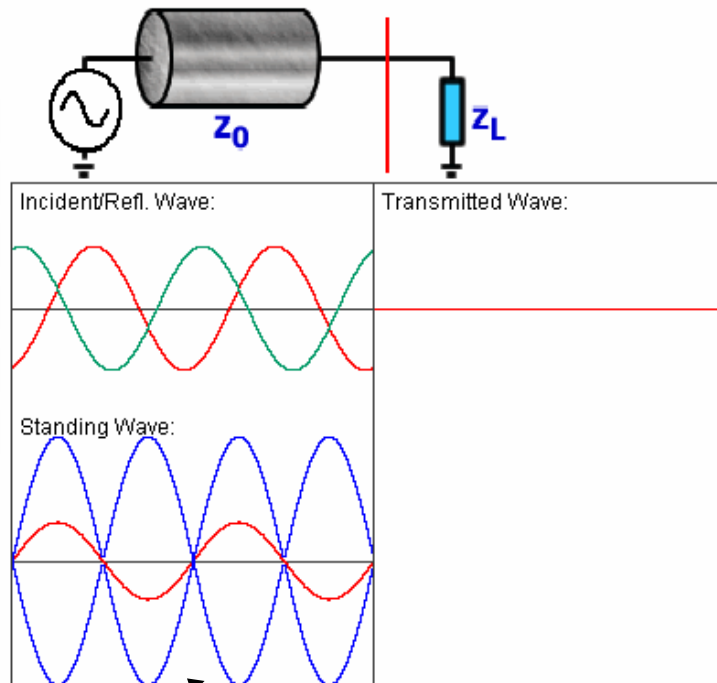
Mismatch Loss (dB)

Z1

er1

Show two interfaces

Resume



Standing Wave

[Besser Associates](#)

Standing Waves

Reflectometer Calculator

Type a value in one of the fields below and hit 'enter:'

Reflection Coefficient

SWR

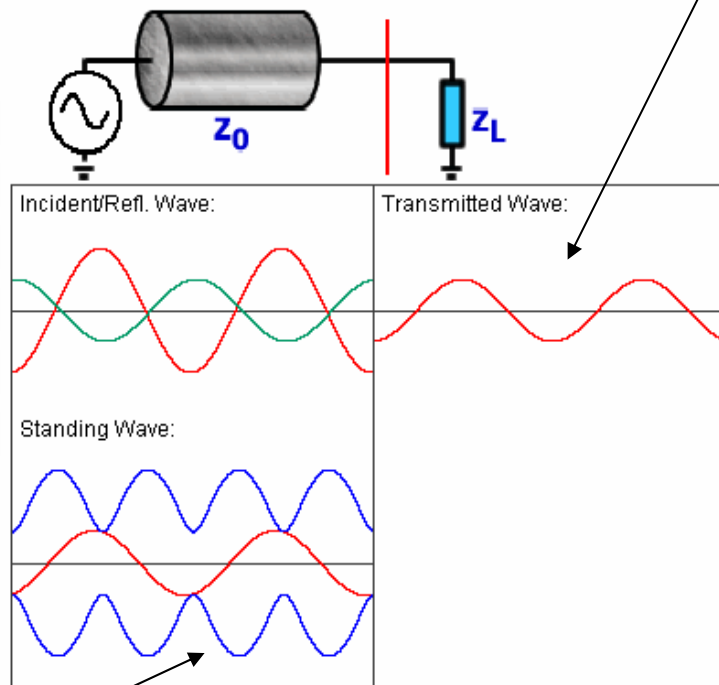
Return Loss (dB)

Mismatch Loss (dB)

Z1

er1

Show two interfaces



This may be wrong
We will see shortly



Standing Wave

[Besser Associates](#)

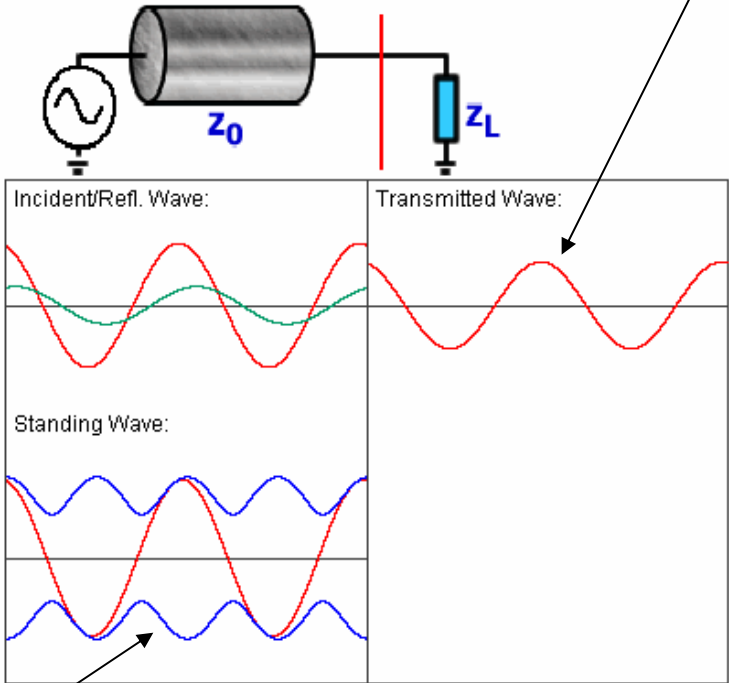
Standing Waves

Reflectometer Calculator

Type a value in one of the fields below and hit 'enter:'

Reflection Coefficient	<input type="text" value="0.301"/>
SWR	<input type="text" value="1.86"/>
Return Loss (dB)	<input type="text" value="10.437"/>
Mismatch Loss (dB)	<input type="text" value="0.412"/>
Z1	<input type="text" value="93"/>
er1	<input type="text" value="1.0"/>

Show two interfaces



This may be wrong
We will see shortly



Standing Wave

[Besser Associates](#)

Standing Waves

AppCAD - [Reflection Calculator] Main Menu [F8]

File Select Parameters Options Help

Reflection Calculator

[From Agilent](#)

$Z_s = 50 \ \Omega$

V_s

$Z_o = Z_s$

Load

$P_i = 10 \text{ mW}$

$P_r = 0.904 \text{ mW}$

$P_t = 9.096 \text{ mW}$

$|\Gamma| = 0.301$
 $Z_l = 93 \ \Omega$
 $Y_l = 0.01075 \text{ mho}$

$SWR = 1.86 : 1$
 Return Loss, RL = 10.437 dB
 Mismatch Loss, Lmm = 0.412 dB
 Transmission Coefficient, T = 0.910 (ratio)
 Transmission Coefficient, T = 0.412 dB

1. Input source impedance, Z_s
2. Input any parameter in the right column. Press Enter (with cursor in the entry field) to calculate remaining reflection parameters.
3. Input any of the three power levels. Press Enter to calculate the other two powers.

Normal [Click for Web: APPLICATION NOTES - MODELS - DESIGN TIPS - DATA SHEETS - S-PARAMETERS](#)

$$\beta = \omega \sqrt{LC}$$

$$= \frac{\omega}{v}$$

Transmission Lines - Standing Wave Derivation

$$(\omega t - \beta z)$$

$e^{j\omega t}$

Phasor Form of the Wave Equation:

$$\frac{\partial^2 V}{\partial z^2} = L \cdot C \cdot \frac{\partial^2 V}{\partial t^2}$$

where:

$$V = V^{\mp} \cdot e^{\pm j \cdot \beta \cdot z}$$

$$\Rightarrow \frac{\partial^2 V}{\partial z^2} = -\omega^2 \cdot L \cdot C \cdot V$$

lossless

General Solution:

$$V = V^+ e^{-j \cdot \beta \cdot z} + V^- e^{+j \cdot \beta \cdot z}$$

Starting Pt

Workspace

$$\beta^2 = \omega^2 \epsilon c$$

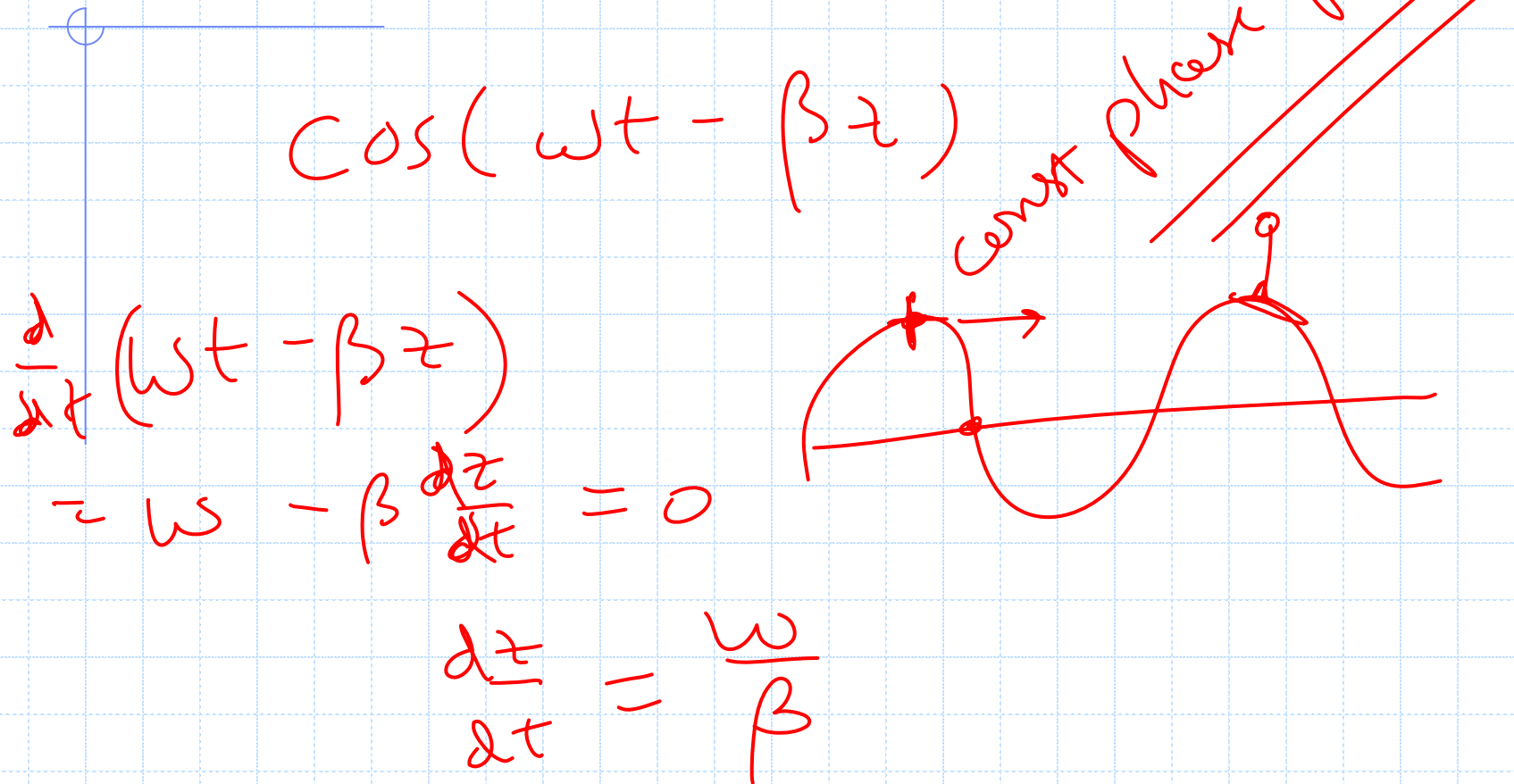
$$\frac{\partial^2 \tilde{V}}{\partial z^2} = -\omega^2 \epsilon c \tilde{V} \quad \frac{\partial}{\partial t} \rightarrow j\omega$$

$$\tilde{V} = \tilde{V}^+ e^{-j\beta z} + \tilde{V}^- e^{+j\beta z}$$

$$\frac{\partial \tilde{V}}{\partial z} = \tilde{V}^+ (-j\beta) e^{-j\beta z}$$

$$\frac{\partial^2 \tilde{V}}{\partial z^2} = \tilde{V}^+ (-j\beta)^2 e^{-j\beta z} = -\tilde{V}^+ \beta^2 e^{-j\beta z} = -\beta^2 \tilde{V}$$

Workspace



Transmission Lines - Standing Wave Derivation

$$V = V^+ e^{-j\beta \cdot z} + V^- e^{+j\beta \cdot z}$$

Forward Wave

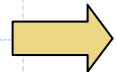
$$\cos(\omega \cdot t - \beta \cdot z)$$

TIME DOMAIN

Backward Wave

$$\cos(\omega \cdot t + \beta \cdot z)$$

V_{\max} occurs when Forward and Backward Waves are in Phase



CONSTRUCTIVE INTERFERENCE

V_{\min} occurs when Forward and Backward Waves are out of Phase



DESTRUCTIVE INTERFERENCE

matched

$$V^- = 0$$

Transmission Lines Formulas

$$\frac{V(z)}{i(z)} = Z_0$$

- [Fields and Waves I Quiz Formula Sheet](#)
- In the class notes

$$v(z) = V_+ e^{-j\beta z} + V_- e^{+j\beta z}$$

$$i(z) = \frac{V_+ e^{-j\beta z} - V_- e^{+j\beta z}}{Z_0} = \frac{V_+}{Z_0} e^{-j\beta z} - \frac{V_-}{Z_0} e^{+j\beta z}$$

- Note: $V_+ = V^+ = V_m^+$ $V_- = V^- = V_m^-$

All are used in various handouts, texts, etc. There is no standard notation.

RG584

$$Z_0 = 50 \Omega$$

RG58/U Cable

$$\frac{2\pi (1.5 \times 10^6)}{2 \times 10^8}$$

- Assume 2 V_{p-p} 1.5MHz sine wave is launched on such a line. Find $\beta = \frac{\omega}{u} = \omega\sqrt{lc} = \omega\sqrt{\mu\epsilon} = \frac{2\pi}{\lambda}$ and λ

$$u = \frac{2}{3}c \cong 2 \times 10^8 \text{ m/s}$$

- Answers?

$$l = .25 \times 10^{-6} \text{ H/m}$$

$$c = 100 \times 10^{-12} \text{ F/m}$$

$$\cos(\omega t - \beta z)$$

$$\beta z = 2\pi$$
$$z = \lambda$$



Reflection Coefficient Derivation

Define the Reflection Coefficient:

$$|V_m^-| = |\Gamma_L| \cdot |V_m^+|$$

Maximum Amplitude when in Phase: $V_{max} = |V_m^+| + |V_m^-|$

$$\therefore V_{max} = |V_m^+| \cdot (1 + |\Gamma_L|)$$

Similarly: $V_{min} = |V_m^+| \cdot (1 - |\Gamma_L|)$

$$\text{Standing Wave Ratio (SWR)} = \frac{V_{max}}{V_{min}} = \frac{1 + |\Gamma_L|}{1 - |\Gamma_L|} = \frac{V^+ (1 + |\Gamma_L|)}{V^+ (1 - |\Gamma_L|)}$$

Transmission Lines - Standing Wave Derivation

Distance between Max and Min is $\lambda/2$   Show this

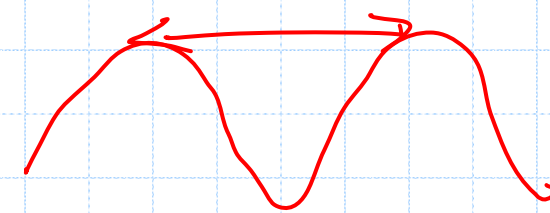
Assume V^{\pm} are real (will be complex if the load is complex)

Forward Phase is = $-j \cdot \beta \cdot z$

Backward Phase is = $+j \cdot \beta \cdot z$

Difference in Phase is = $-2 \cdot j \cdot \beta \cdot z$

Varies by 2π (distance between maxima)

$$\therefore 2 \cdot \beta \cdot \Delta z = 2 \cdot \pi \quad \Rightarrow \quad \Delta z = \frac{\pi}{\beta} = \frac{\pi}{2 \cdot \pi / \lambda} = \frac{\lambda}{2}$$


Reflection Coefficient Derivation

Let $z=0$ at the LOAD

$$\begin{aligned}\Rightarrow V_{load} &= V^+ \cdot e^{-j\beta \cdot 0} + V^- \cdot e^{+j\beta \cdot 0} \\ &= V^+ + V^- \\ &= V^+ \cdot (1 + \Gamma_L)\end{aligned}$$

Need a relationship between current and voltage:

$$\frac{\partial V}{\partial z} = -l \cdot \frac{\partial I}{\partial t} \quad \Rightarrow \quad \frac{\partial V}{\partial z} = -j \cdot l \cdot \omega \cdot I$$

Reflection Coefficient Derivation

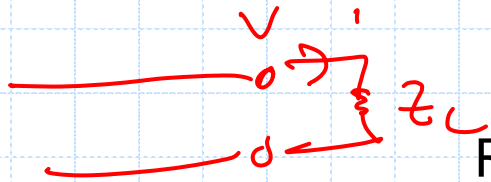
$$I = -\frac{l}{j \cdot \omega \cdot l} \cdot \frac{\partial V}{\partial z}$$

$$= -\frac{1}{j \cdot \omega \cdot l} \cdot (-j \cdot \beta \cdot V^+ \cdot e^{-j \cdot \beta \cdot z} + j \cdot \beta \cdot V^- \cdot e^{+j \cdot \beta \cdot z})$$

$$= \frac{\beta}{\omega \cdot l} \cdot (V^+ \cdot e^{-j \cdot \beta \cdot z} - V^- \cdot e^{+j \cdot \beta \cdot z})$$

$$\therefore I = \frac{\omega \cdot \sqrt{l \cdot c}}{\omega \cdot l} \cdot (V^+ \cdot e^{-j \cdot \beta \cdot z} - V^- \cdot e^{+j \cdot \beta \cdot z})$$

$$= \frac{V^+}{\sqrt{\frac{l}{c}}} \cdot e^{-j \cdot \beta \cdot z} - \frac{V^-}{\sqrt{\frac{l}{c}}} \cdot e^{+j \cdot \beta \cdot z} = \frac{V^+}{\sqrt{\frac{l}{c}}} \cdot e^{-j \cdot \beta \cdot z} - \frac{V^+ \cdot \Gamma_L}{\sqrt{\frac{l}{c}}} \cdot e^{+j \cdot \beta \cdot z}$$



Reflection Coefficient Derivation

$$V(z)$$

$$I(z)$$

At LOAD: $\frac{V}{I} = Z_L$

$$\leftarrow \frac{V(\text{load})}{I(\text{load})} = Z_L$$

Use derived terms of V and I at $z=0$ (position of the LOAD)

$$e^{-j\beta z}$$

$$e^{+j\beta z}$$

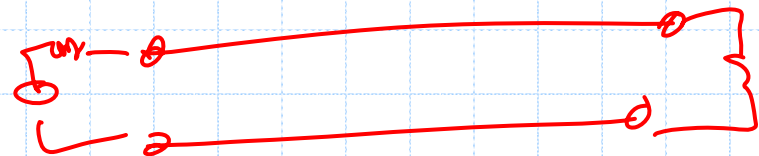
$$\left(\frac{V^+}{\sqrt{l/c}} - \frac{V^+ \cdot \Gamma_L}{\sqrt{l/c}} \right)^{-1} \cdot (V^+ + \Gamma_L \cdot V^+) = Z_L$$

$$Z_L = \sqrt{\frac{l}{c}} \cdot \left(\frac{1 + \Gamma_L}{1 - \Gamma_L} \right)$$

Note that $Z_0 = \sqrt{\frac{l}{c}}$

OR

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$



Short Circuit Load

$$Z \equiv [1 : 10] Z_0$$

■ For $Z_L = 0$, we have $\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{0 - Z_0}{0 + Z_0} = -1$

$$v(z) = V^+ e^{-j\beta z} + \Gamma_L V^+ e^{+j\beta z} = V^+ (e^{-j\beta z} - e^{+j\beta z})$$

$$e^{+j\beta z} = \cos \beta z + j \sin \beta z$$

$$e^{-j\beta z} = \cos \beta z - j \sin \beta z$$



$$v(z) = -V^+ (j2 \sin \beta z)$$

Standing Wave

Short Circuit Load

- Convert to space-time form

$$v(z, t) = \operatorname{Re}\left(v(z)e^{j\omega t}\right) = \operatorname{Re}\left(V^+(-j2 \sin \beta z)e^{j\omega t}\right)$$

$$\operatorname{Re}\left((-j2 \sin \beta z)e^{j\omega t}\right) = \operatorname{Re}\left(-2 \sin \beta z(j \cos \beta z - \sin \beta z)\right)$$

$$v(z, t) = 2V^+ \sin \beta z \sin \omega t$$

- This is a standing wave

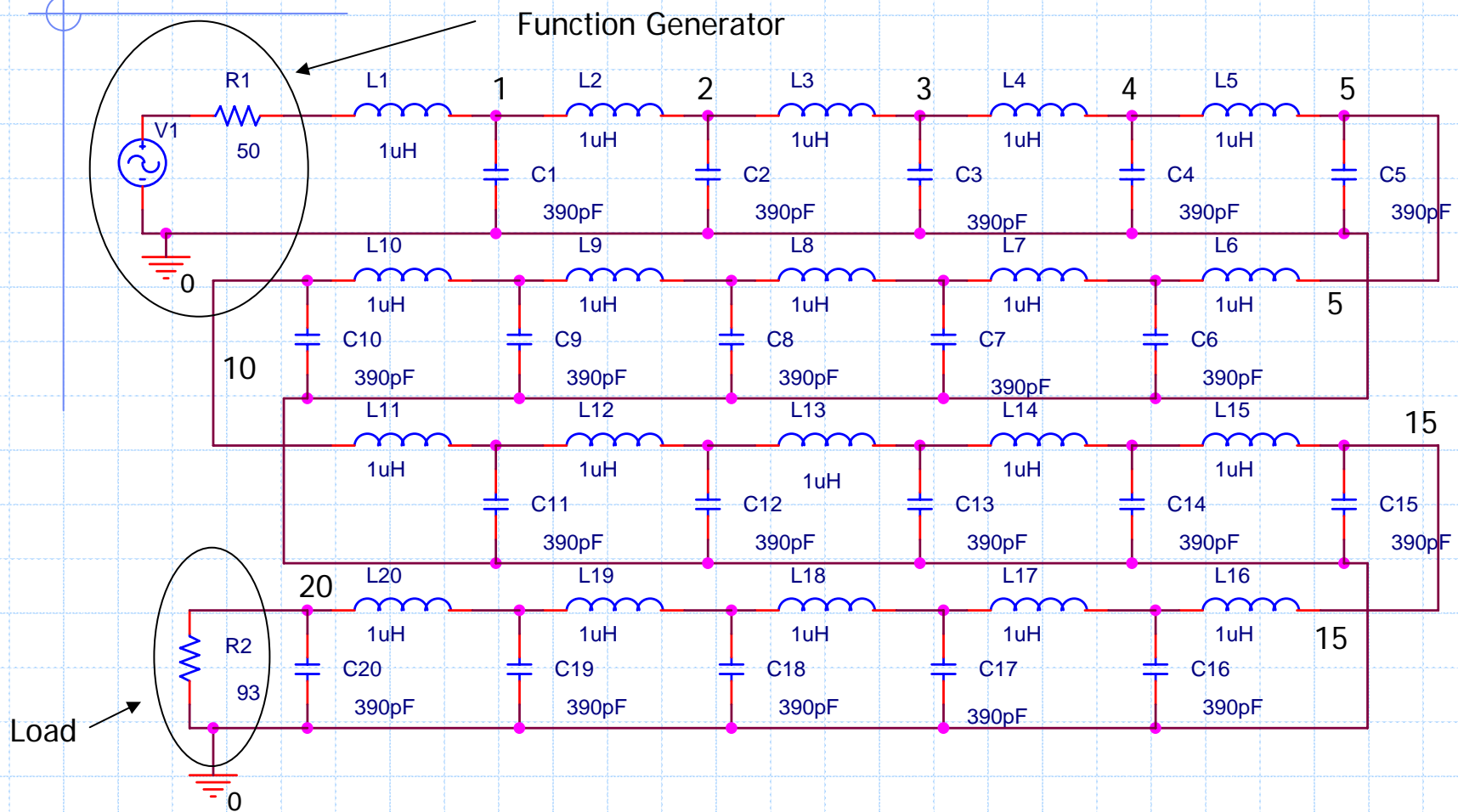
Short Circuit Load

- What are the voltage maxima and minima?

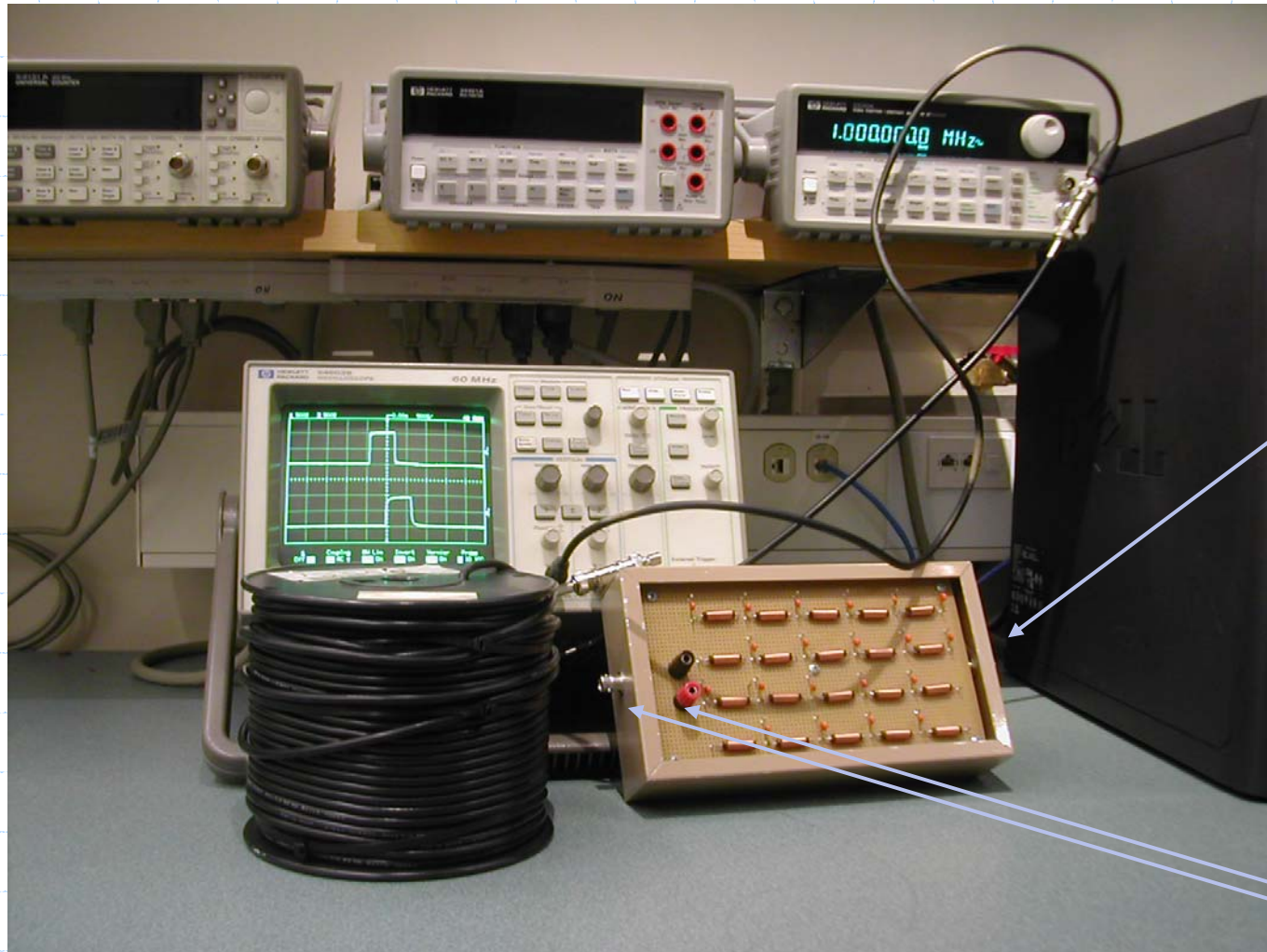
$$v(z, t) = 2V^+ \sin \beta z \sin \omega t$$

- Where are they?
- The standing wave pattern is the envelope of this function.

Lumped Transmission Line



Lumped Transmission Line



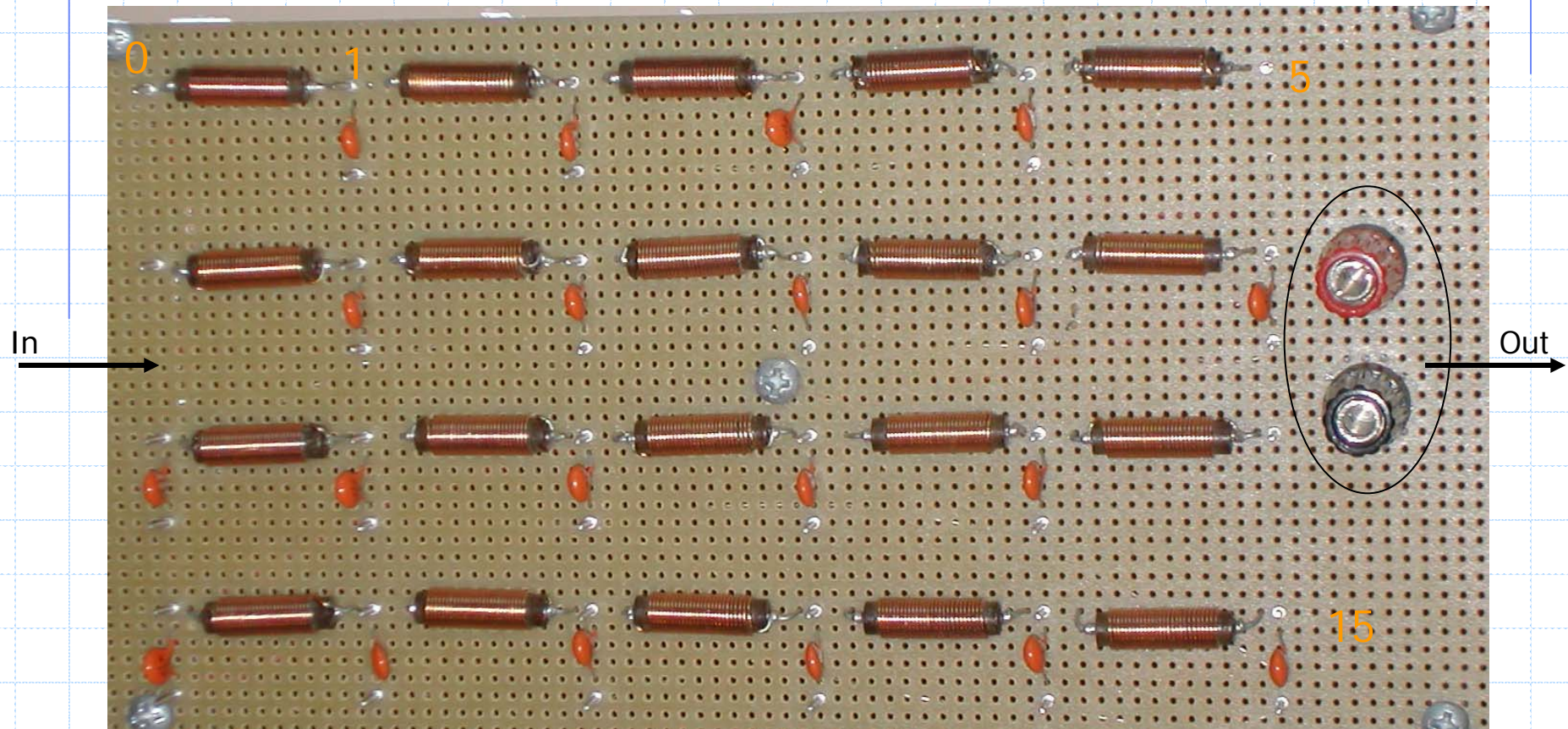
Input Not
Shown

Both
Outputs
Shown

Lumped Transmission Line

Input is BNC

Output is both BNC and Banana Plugs (for some loads)



Lumped Transmission Line Experiment

- Treat the lumped version just like the reel of cable. (Connectors are opposite so you will need connector cables.)
- Monitor the output of the function generator on one channel
- Monitor the voltages on each node (one at a time) on the other channel. You can use just the signal (red) lead, since the ground (black) lead is connected through the other cables. Use the voltage cursors to obtain V_{p-p} for each node. Record your values and plot with Excel, Matlab, etc.

Lumped Transmission Line Numerical Experiment (Not required)

- Use PSpice to set up the standard transmission line, matched and not
- Look at the output for a variety of frequencies
- Set up the lumped line in PSpice (more work) and repeat
- Use the lumped line model to show the standing wave pattern
- Will there be any obvious differences between the physical and numerical experiments?

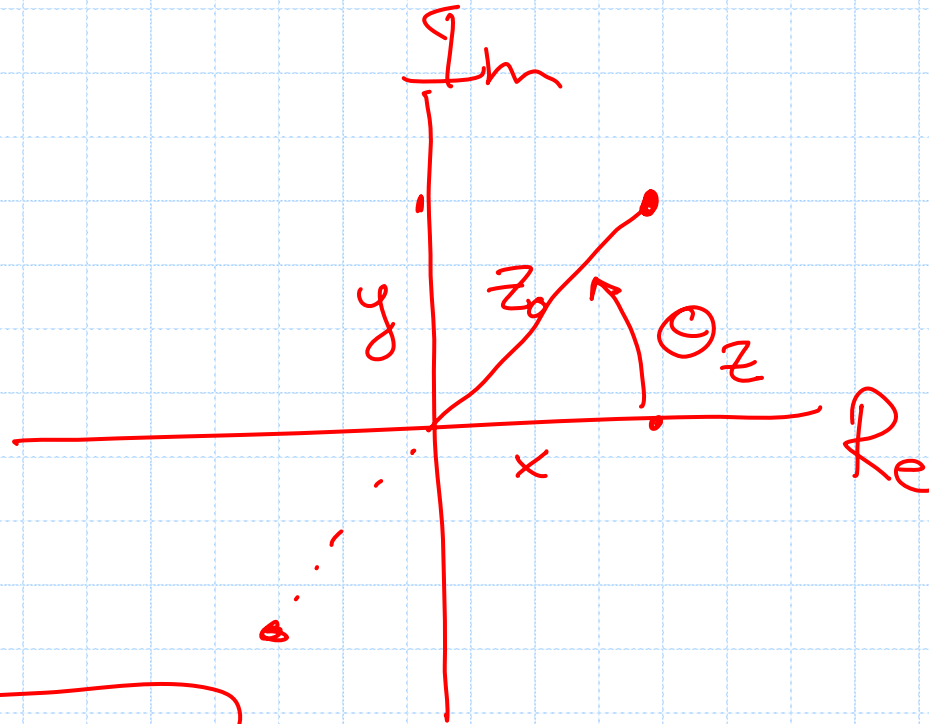
Workspace

$$z = z_0 e^{j\theta_z}$$

$$= x + jy$$

$$z_0 = \sqrt{x^2 + y^2}$$

$$\theta_z = \arctan \frac{y}{x}$$



Workspace

$$\frac{d}{dt} e^{j\omega t} = j\omega e^{j\omega t}$$

$$V(z) = V^+ e^{-j\beta z} + V^- e^{+j\beta z}$$

$$\frac{\partial i}{\partial t} = -c \frac{\partial V}{\partial z}$$

$$\frac{\partial V}{\partial z} = -l \frac{\partial i}{\partial t}$$

c cap/length

l ind/length

$$\frac{d}{dt} \rightarrow j\omega$$

$$\frac{\partial V}{\partial z} = -j\omega l i$$

Workspace

$$\beta = \omega \sqrt{\mu \epsilon} \quad Z_0 = \frac{\omega \mu}{\beta} = \frac{\omega \mu}{\omega \sqrt{\mu \epsilon}}$$

$$i = \frac{-1}{j\omega l} \frac{\partial V}{\partial z}$$

$$V = V^+ e^{-j\beta z} + V^- e^{+j\beta z}$$

$$\frac{\partial V}{\partial z} = V^+ (-j\beta) e^{-j\beta z} + V^- (j\beta) e^{+j\beta z}$$

$$i(z) = V^+ \frac{j\beta}{j\omega l} e^{-j\beta z} - \frac{j\beta}{j\omega l} e^{+j\beta z} V^-$$
$$= \frac{V^+}{Z_0} e^{-j\beta z} - \frac{V^-}{Z_0} e^{+j\beta z}$$

Workspace

$$V(z) = V^+ e^{-j\beta z} + V^- e^{+j\beta z}$$

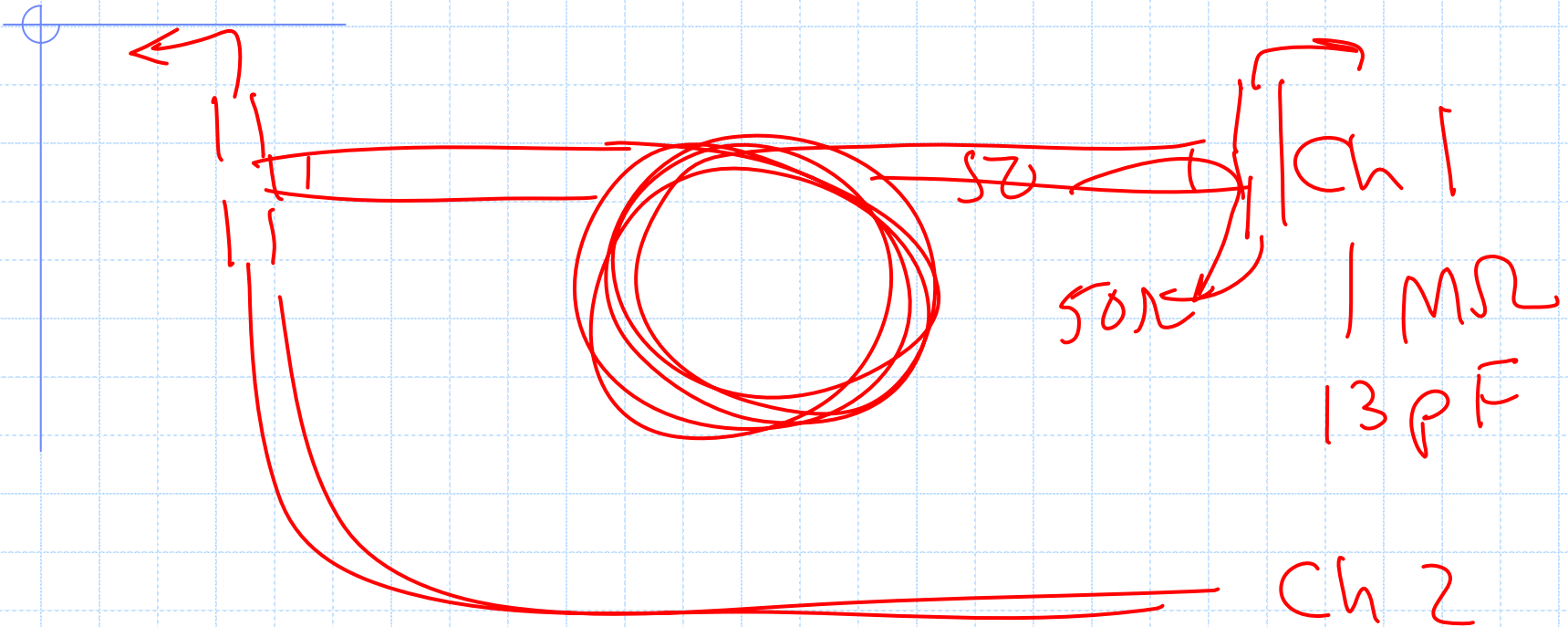
$$I(z) = \frac{V^+}{Z_0} e^{-j\beta z} - \frac{V^-}{Z_0} e^{+j\beta z}$$

$$Z_0 = \sqrt{\frac{\mu}{\epsilon}} \quad \beta = \omega \sqrt{\mu \epsilon}$$

$$V^- = \Gamma_L V^+$$

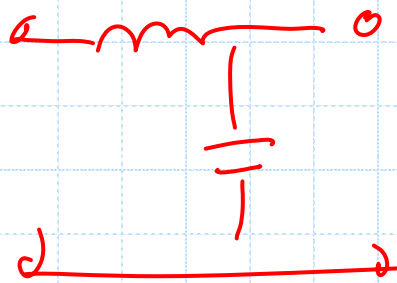
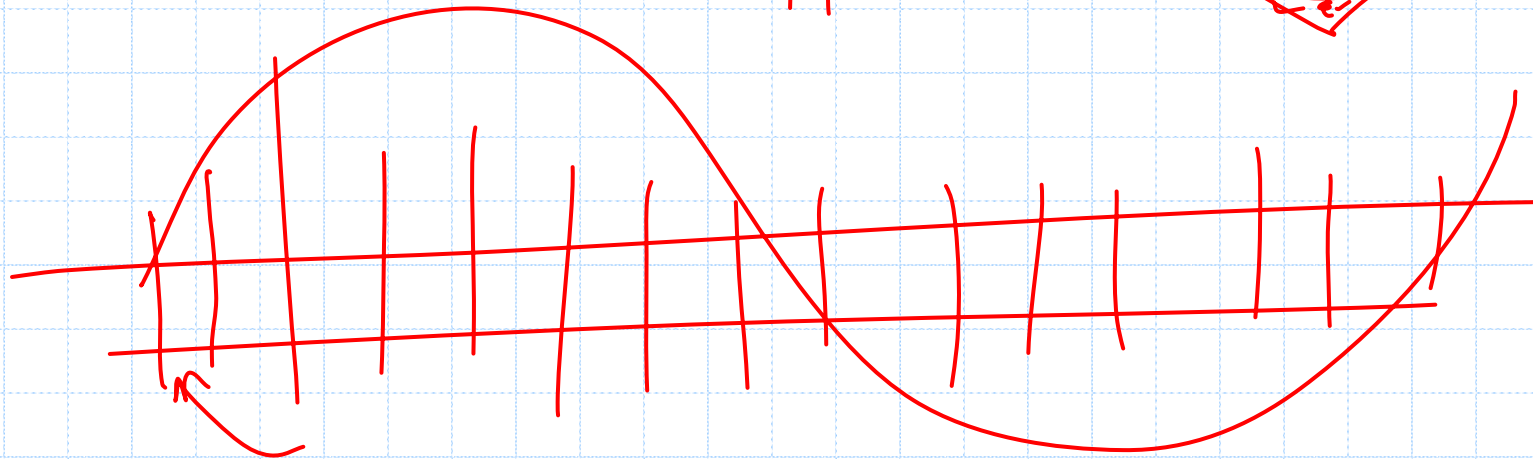
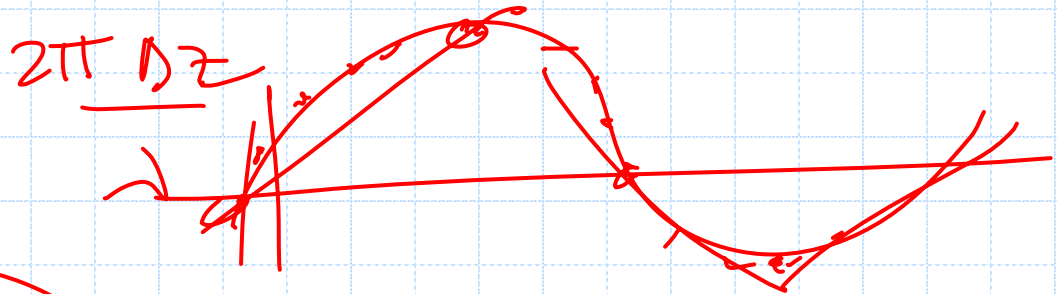
Workspace

$$u = 2 \times 10^8 \text{ m/s}$$



Workspace

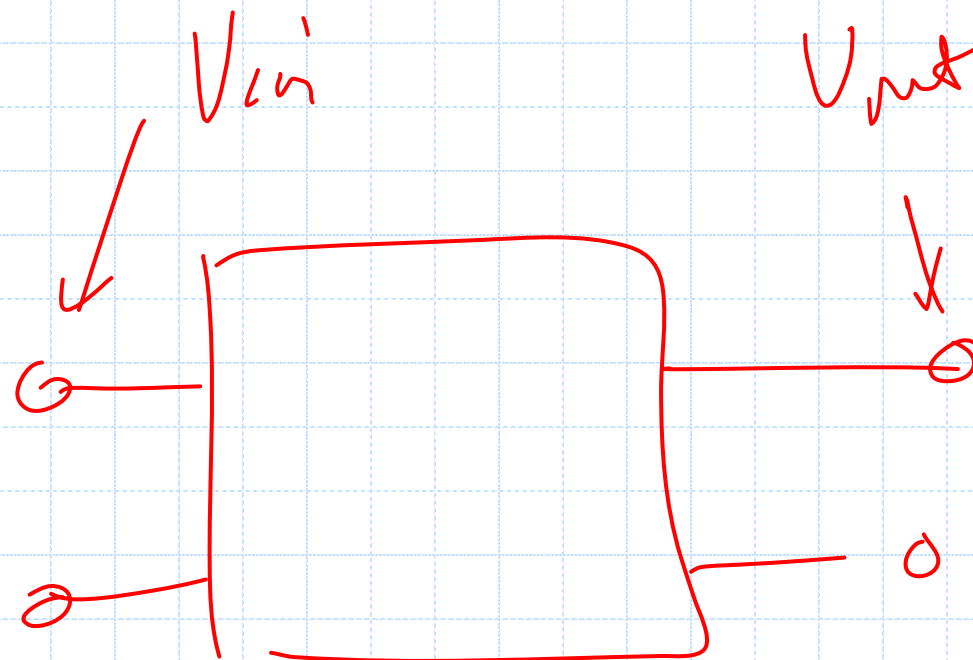
$$\beta = \frac{2\pi}{\lambda}$$



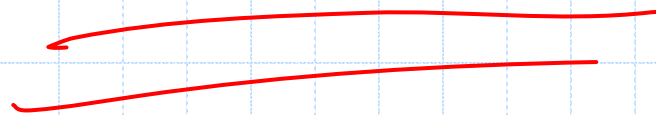
$$\Delta z \ll \lambda$$

$$\frac{\cos(\beta z) \sin(\beta z)}{\sin \beta \Delta z} \approx \beta \Delta z$$

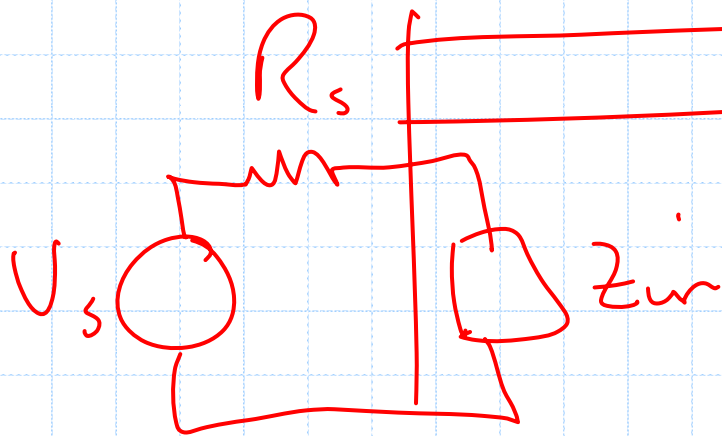
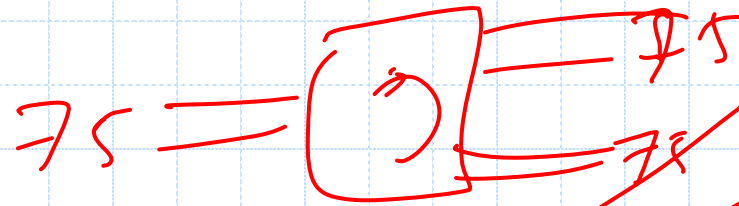
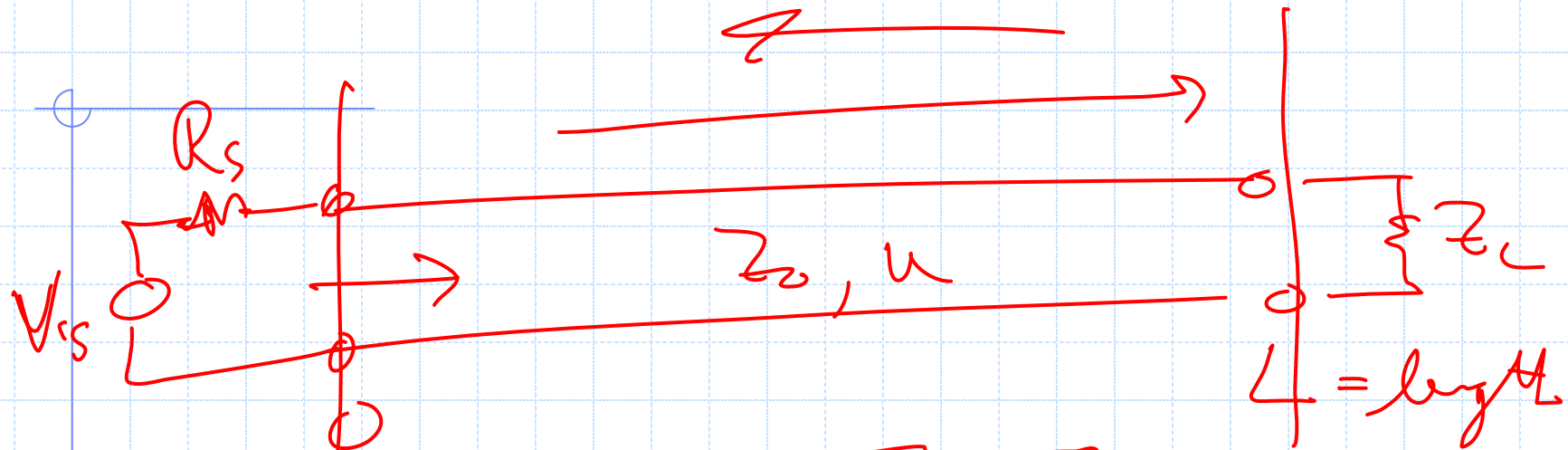
Workspace



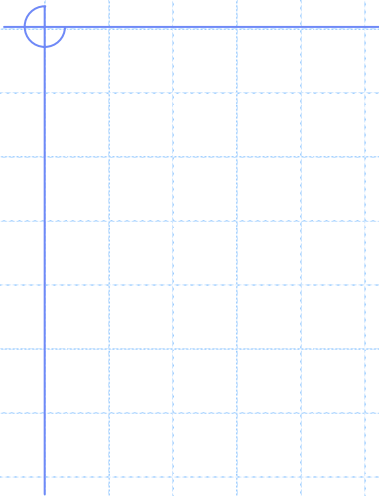
Monitor Both



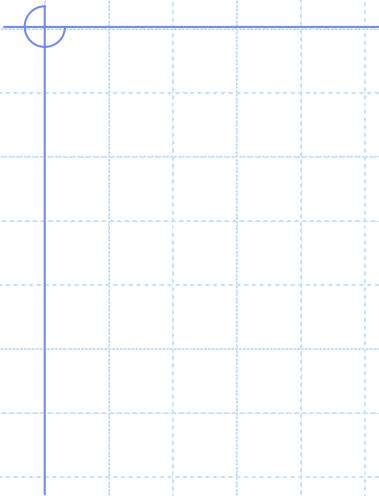
Workspace



Workspace



Workspace



Workspace

