

$$1. \quad a) \quad l = \frac{\mu_0}{2\pi} \ln \frac{b}{a} = \frac{4\pi \times 10^{-7}}{2\pi} \ln \frac{1.4}{.4} = 2.5 \times 10^{-7} \text{ H/m}$$

$$C = \frac{2\pi \epsilon}{\ln b/a} = \frac{2\pi (2.25) \frac{1}{36\pi} \times 10^{-9}}{\ln \frac{1.4}{.4}} = 10^{-10} \text{ F/m}$$

$$v = \frac{1}{\sqrt{\mu_0 \epsilon}} = \frac{2}{3} c = 2 \times 10^8 \text{ m/s}$$

$$Z_0 = \sqrt{\frac{\mu}{\epsilon}} \frac{\ln b/a}{2\pi} = 50 \Omega$$

$$b) \quad l = 800 \text{ turns large} \Rightarrow l = 2 \times 10^{-4} \text{ H/m}$$

$$C = \frac{2\pi (4) \epsilon_0}{\ln b/a} = 10^{-10} \frac{4}{2.3} = 1.7 \times 10^{-10} \text{ F/m}$$

$$v = \frac{1}{\sqrt{4 \cdot 800}} c = 5.3 \times 10^6 \text{ m/s}$$

$$Z_0 = \sqrt{\frac{800 (2.25)}{4}} 50 \approx 1000 \Omega$$

c) Any reasonable reference accepted

2. Reluctance of the empty cylindrical hole

$$\text{empty: } R_1 = \frac{d}{\mu_0 \pi a^2}$$

$$\mu = \mu_r \mu_0$$

in iron

Washer-like regions at the ends

$$R_2 = R_4 = \int_a^c \frac{dr}{\mu (2\pi r t)}$$

$$= \frac{1}{\mu 2\pi t} \int_a^c \frac{dr}{r}$$

$$= \frac{1}{\mu 2\pi t} \ln \frac{c}{a}$$

For the outer cylinder

$$R_3 = \frac{d - 2t}{\mu \pi (c^2 - b^2)} \approx \frac{d}{\pi \mu (c^2 - b^2)}$$

$$\phi = \frac{NI}{R_1 + R_2 + R_3 + R_4}$$

$$\Lambda = N\phi = LI$$

$$L = \frac{N^2}{R_1 + R_2 + R_3 + R_4} \approx \frac{N^2 \mu_0 \pi a^2}{d}$$

↑ dominant term.

b.  $R_i$  is now  $\frac{d}{\mu \pi a^2}$  so all 4 terms are important

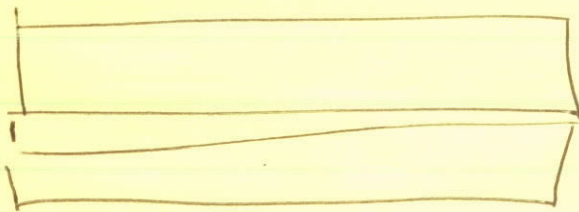
$$\phi = \frac{NI}{\sum R_i}$$

$$\Lambda = LI = \frac{N^2}{\sum R_i}$$

c. Energy =  $\frac{1}{2} LI^2$

d.  $W_m = \frac{1}{2} I^2 \left( L_{\text{empty}} + \Delta L \frac{x}{d/2} \right)$

$$F = -\nabla W_m = \frac{1}{2} I^2 \frac{\Delta L}{d/2}$$

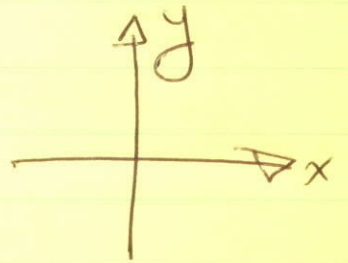


$$L_{\text{max}} = \Delta L + L_{\text{empty}}$$

e. any reasonable material. Note that  $\mu$  for iron is usually nonlinear so a typical value is 0.00

$$3. a. \vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\phi}$$

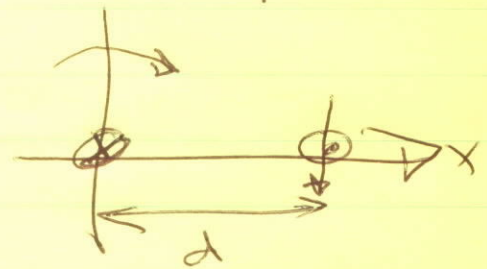
$$= -\frac{\mu_0 I}{2\pi d} \hat{y}$$



$$b. \vec{F} = I L \vec{B} \hat{x}$$

$$= I \frac{\mu_0 I}{2\pi d} \hat{x}$$

$$= \mu_0 \frac{I^2}{2\pi d} \hat{x}$$



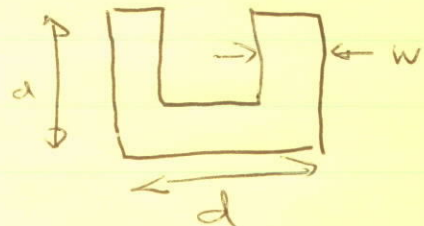
per unit length  
 $L=1$

c. The force is repulsive

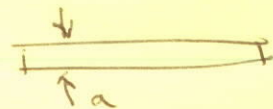
The force goes as  $\vec{J} \times \vec{B}$

4. a. First find the reluctance

$$R_{\text{core}} = \frac{3d}{\mu w^2}$$



$$R_{\text{plate}} = \frac{d}{\mu a w}$$



$$R_{\text{gap}} = \frac{g}{\mu_0 w^2}$$

$$R = \sum R_i = R_{\text{core}} + R_{\text{plate}} + 2 R_{\text{gap}}$$

$$\text{Now } \Lambda = N\phi = LI$$

$$\phi = \frac{N_1 I}{\mathcal{R}} \approx \frac{N_1 I}{2\mathcal{R}_{\text{gap}}}$$

$$\Lambda \approx \frac{N_1^2 I}{2\mathcal{R}_{\text{gap}}} \approx \frac{N_1^2 I \mu_0 \omega^2}{2g}$$

$$\Rightarrow L_1 \approx \frac{N_1^2 \mu_0 \omega^2}{2g}$$

b.  $\phi$  done above

$$\begin{aligned} \phi &= \frac{N_1 I}{\mathcal{R}} \\ &\approx \frac{N_1 I}{2\mathcal{R}_{\text{gap}}} \end{aligned}$$

$$\Lambda_{21} \approx \frac{N_2 N_1 I}{2\mathcal{R}_{\text{gap}}} \approx \frac{N_1 N_2 I \mu_0 \omega^2}{2g}$$

$$c. \Lambda_{21} \approx \frac{N_1 N_2 I \mu_0 \omega^2}{2g(t)}$$

$$g(t) = g_0 \cos \omega t$$

$$d. V = -\frac{d\Lambda_{21}}{dt} = -\frac{N_1 N_2 I \mu_0 \omega^2}{2} \frac{d}{dt} g^{-1}$$

$$\frac{d}{dt} g^{-1} = g^{-2} \frac{dg}{dt} = \frac{-\omega g_0 \sin \omega t}{g_0^2 \cos^2 \omega t}$$

This is not a very practical measurement since the voltage can be very large (with  $\cos^2 \omega t$  in the denominator). Practically, one can add an integrator circuit to the output and losses would keep the voltages finite.

